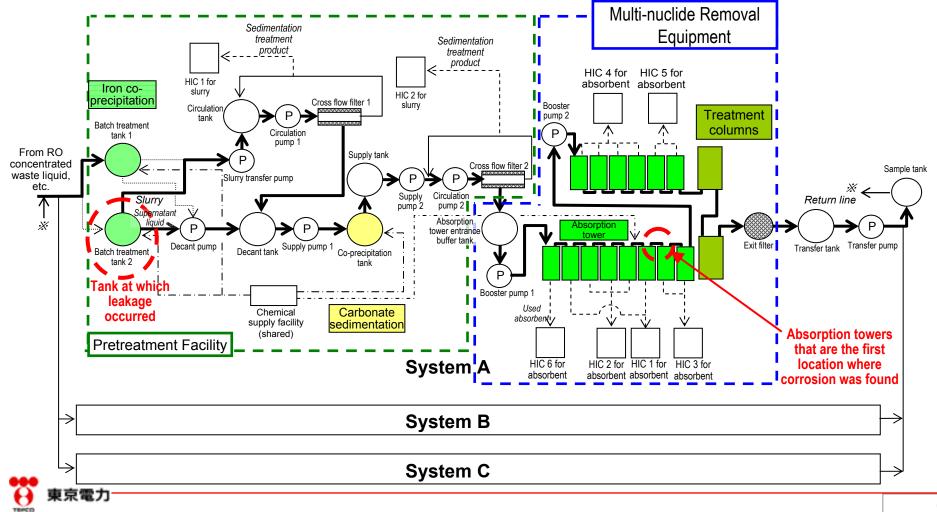
<Reference> September 25, 2013 Tokyo Electric Power Company

## Cause and Preventive Actions Following Leakage from a Batch Treatment Tank of Multi-nuclide Removal Equipment

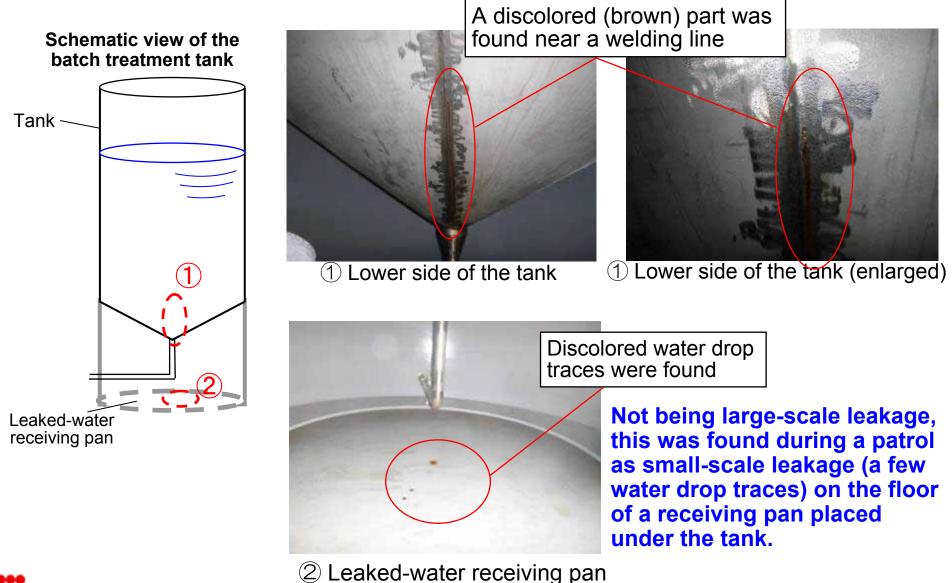


# **Locations of Leakage and Corrosion**

- On June 15, leakage from the lower side of the batch treatment tank 2A was found.
- In a horizontally deployed investigation conducted later, corrosion was found in some locations including the absorption tower 6A



## **Results of Leakage from the Batch Treatment Tank 2A**



# **Causes of Leakage and Corrosion**

Leakage from the lower side of the batch treatment tank 2A

Unexpectedly damaging corrosion was caused by a combination of complex factors such as **formation of a crevice environment** due to accumulation and adhesion of generated iron precipitation on the internal surface of the tank, and **development of a corrosive environment** due to injection of chemicals (mainly, hypochlorous acid). A through-hole was made at a corroded part, causing the leakage.

Corrosion in the absorption tower 6 and further downstream locations

While **silver impregnated activated carbon** with which the absorption tower 6 is filled is considered to **contribute to occurrence and development of corrosion**, corrosion was found in locations downstream of the absorption tower 6 that are not in the alkaline environment.

Corrosion near the batch treatment tank and at flange parts of the absorption tower 6 and further downstream locations
Around each of the flange parts where corrosion was found, fluid becomes stagnant due to the shape of the flange part, and flows slowly, which is favorable for local corrosion to occur. This is considered as another factor contributing to development of corrosion.



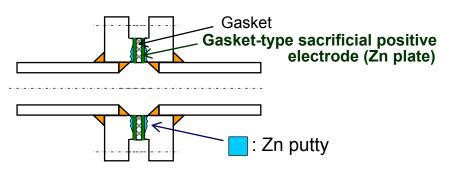
## **Recurrence Prevention Measures on Batch Treatment Tanks and Horizontal Deployment**

#### Recurrence prevention measures on batch treatment tanks

After the damaged parts were repaired, **rubber lining (chloroprene rubber) was provided** on the internal surfaces of the tanks.

Measures taken within the horizontal deployment range

Gasket-type sacrificial positive electrodes, etc., were provided to flanges that have the risk of suffering crevice corrosion. Additionally, for higher reliability, we are considering future replacement with lining pipes.





Batch treatment tank 1C (after rubber lining was provided)



Gasket-type sacrificial positive electrode



#### Preventive Actions for Starting a Hot Test for the System C in Response to the Occurrence of Corrosion in Absorption Towers

### Stop injection of hypochlorous acid

- Bypass the silver impregnated activated carbon tower in a neutral region where a corrosion potential is increased.
- Consider restructuring of absorption towers in order to secure the absorption capability expected from silver impregnated activated carbon, which is to be bypassed.
- After the start of the hot test, regularly inspect locations corresponding to those in the system A where relatively severe corrosion was found, so that the corrosion suppression effects of the respective corrosion prevention measures, in addition to the removal capability, will be checked for extension of our knowledge.

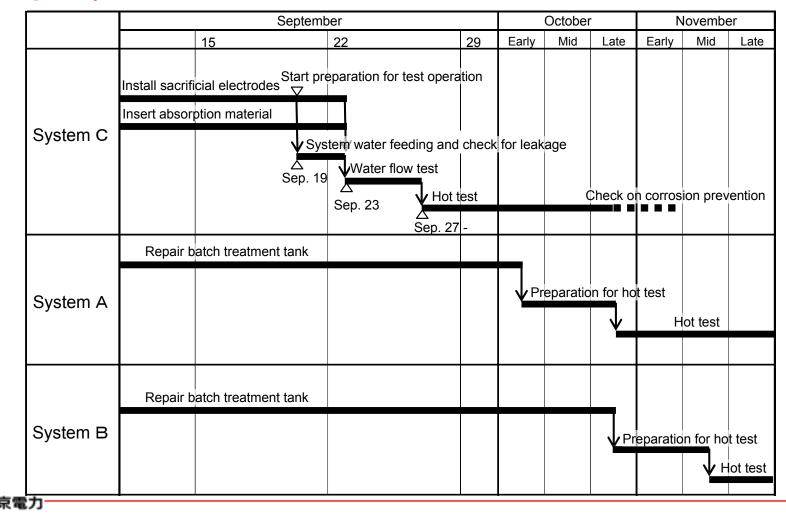
We will take the above actions in order to reduce as early as possible the risk of leakage from the RO concentrated water storage tank, and will start a hot test for the system C on September 27.

Further, we will restart hot tests for the systems A and B as soon as we are ready.



## Schedule

Corrosion prevention work (installation of sacrificial electrodes), absorbent insertion, and water feeding into the system (from Sep. 19) are conducted simultaneously. A water flow test (from Sep. 23) and then <u>a hot test (from Sep. 27)</u> are scheduled to follow.



# (Reference) Structures of Towers at the Start of a Hot Test for the System C

